

Tutorial

Final and Forward Construction Stage Analysis for a PC Cable-Stayed Bridge (Part I)

Civil

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Summary

Cable-stayed bridges are structural systems effectively composed of cables, main girders and towers. This bridge type has a beautiful appearance and easily blends in with the surrounding environment due to the fact that various structural systems can be created by changing the tower shapes and cable arrangements.

Cable-stayed bridges are of a bridge type where inclined cables transfer member forces induced in the girder. High compression is induced in the tower and main girder due to the structural system. Considering the above features, PC cable-stayed bridges using Prestressed Concrete materials for the main girders have the following advantages:

- High buckling resistance compared to steel cable-stayed bridges due to high stiffness of the towers and main girders
- High wind and earthquake resistance compared to steel cable-stayed bridges due to heavier weights, higher stiffness and higher damping ratio
- Concrete cable-stayed bridges are better than steel cable-stayed bridges in terms of serviceability as the stiffness of main girders is large, and thus the deflection due to live loads is relatively small (resulting in good control of noise/vibration).
- Low cost and easy maintenance compared to steel cable-stayed bridges
- Efficient constructability because it essentially consists of cantilevers, and can be built by constructing out from the towers.
- Economical because the minimized girder depths allow more space under the bridges and this type of bridges allows shorter approach length.

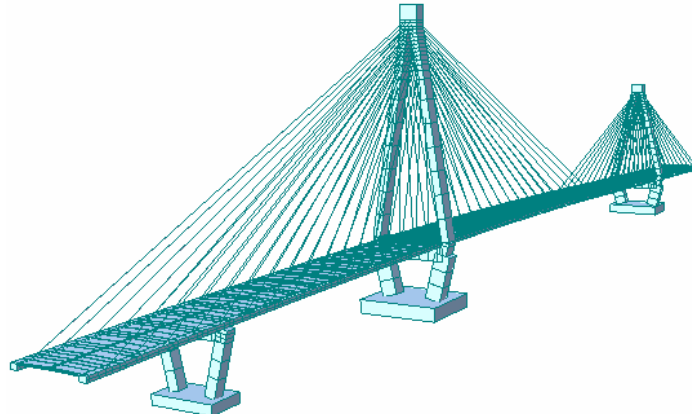


Figure 1. Cable-stayed Bridge

Initial cable pretension analysis considering construction stages

The dominant issue of the design and construction of a cable-stayed bridge is to compute and achieve the initial equilibrium configuration at the completed state. The initial equilibrium configuration of a cable-stayed bridge is the equilibrium position due to dead load and tension forces in the stay cables. It is called “initial cable pretension analysis” to optimize the cable pretensions in order to improve section forces in the main girders and towers and support reactions in the bridge.

In order to guide the construction of each erection stage, backward analysis is commonly adopted, in which the bridge is disassembled stage by stage from the completed state until just before the first pairs of cables are jacked. The forward analysis starting from any construction stage will predict the states in the successive stages by simulating the actual construction procedures.

This tutorial uses an example of a non-symmetrical cable-stayed bridge. Ideally in backward stage analysis, at key segment closure, shear force and bending moment should be close to 0. However, if backward analysis is applied in this case, non-zero shear force and bending moment will occur due to non-symmetry. Thus, it is not desirable to apply backward stage analysis in this case. In addition, with backward stage analysis, time dependent material effects of concrete cannot be considered. Errors due to concrete construction with the time effect can be eliminated by forward iteration analysis. Sequential tensioning and erection sequence, as shown in Figure 2, cannot be represented by backward analysis.

On the other hand, forward stage analysis follows the real erection sequence. It takes more time for the designer as he/she has to conduct trial-and-error analysis to

determine the limiting member forces due to cable tension up to a certain range.

In this tutorial, forward stage analysis is used. In the forward stage analysis, it is necessary to know the cable pretensions at each construction stage, which produce the initial equilibrium configuration at the completed state due to dead load.

Figure 3 shows the sequence for initial cable pretension analysis while considering construction stages.

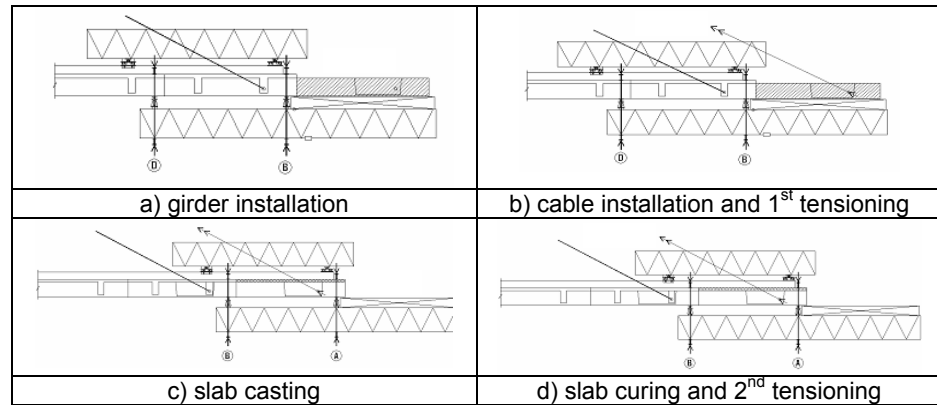


Figure 2. Construction Stage Cycle

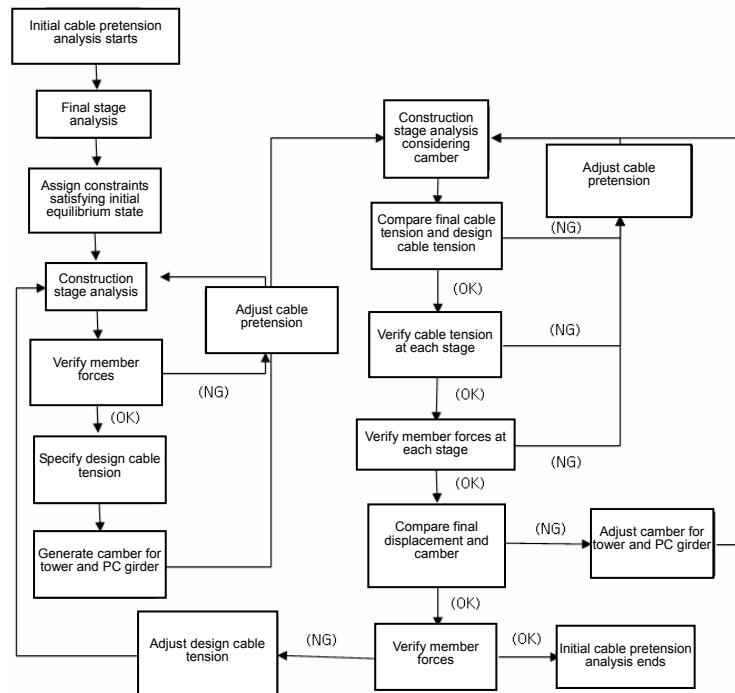


Figure 3. Flow chart for the initial cable pretension analysis considering construction stages

Bridge dimensions

This tutorial has been based on a real project of a PC cable-stayed bridge, and has been simplified since it will still suffice for training purposes. We will learn how to calculate the initial forces in the cables from this tutorial. Before performing initial cable pretension analysis with Construction Stages, initial cable forces due to the dead load at the final stage should be first calculated.

The figures and loadings for the bridge are as follows:

Bridge type: PC cable-stayed bridge
Bridge length: $L = 46.5 + 113.5 + 260.0 + 100.0 = 520.0$ m
2 sides of cables, diamond shape tower
Main girder: Beam and Slab type concrete sections
Tower: concrete sections
Number of cables: 52×2 sides = 104
Install 4 Key blocks in spans 1, 2, 3 & 4
Place 2 elastic bearings on PY1 & PY2

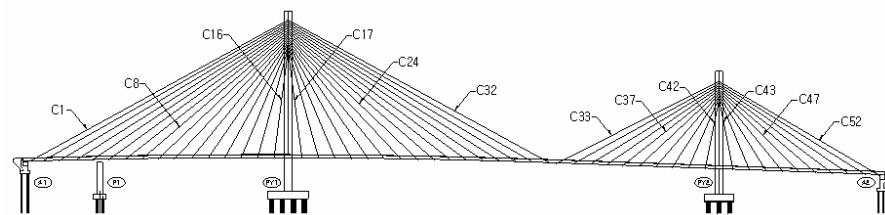


Figure 4. General Layout of Bridge Structure

Loading

Self Weight

Automatically calculated by the program



► Superimposed dead load.

	Unit weight (kN/m)	Remarks
Pavement	35.75	2.3 x 0.08 x 19.43
Railing	7.28	-
Parapet	14.76	-
Sum	57.75	




Self weight of cross beams.

Enter the weight of cross beams, which were excluded in the modeling, using Nodal Loads.

Work Environment Setting

To perform the analysis of a PC cable-stayed bridge, open a new file ( **New Project**) and save it ( **Save**) under the name '**PC.mcb**'.

Assign '**kN**' for Force (Mass) unit and '**m**' for Length unit. This unit system can be changed at any time during the modeling process as desired by the user.

 The Status Bar is located at the bottom of the screen and the units can be changed by clicking on it ( ).

File /  **New Project**

File /  **Save (PC)**

Tools / **Unit System** 

Length > **m** ; Force > **kN** ↵

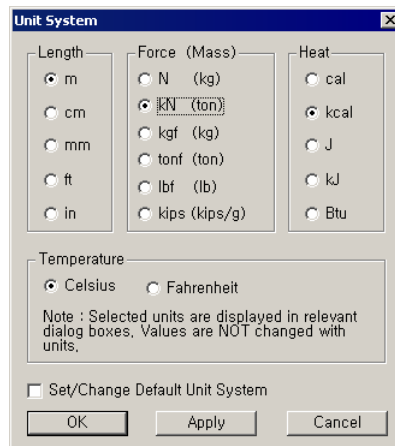


Figure 5. Assign Unit System

Definition of Properties (Attributes)

Definition of Material Properties

Input material properties of cables and bridge deck in the Material Data dialog box.

[Unit : kN, m]

ID	Name	Type of Design	Standard	Modulus of Elasticity	Poisson's Ratio	Thermal Coefficient	Weight Density
1	Main	Concrete	None	2.7389e7	0.167	1.0e-5	24.52
2	Sub	Concrete	None	2.6063e7	0.167	1.0e-5	24.52
3	Cable	Steel	None	2.0594e8	0.3	1.2e-5	76.98

Model / Properties /  **Material**

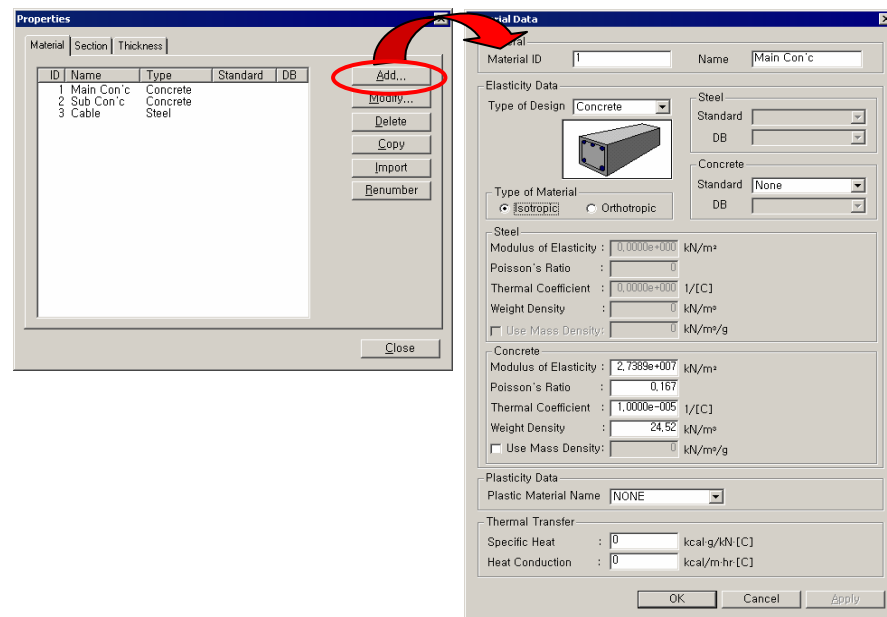


Figure 6. Material Property Input Dialog Box

Definition of Section Properties

With Section Property Calculator (SPC), section properties for an irregular shape can be easily obtained and even the shape can be displayed. Import the *.sec file drawn in SPC to define the main girder sections (101, 102 and 103).

Model / Properties /  **Section**

PSC tab > General Section

Section ID (101) ; Name (D_center)

Click on  button and invoke "D_center.sec".

Referring to the guide diagram, enter the design parameters in the "Param. for Design Input" cell. These parameters are used for section capacity check, but not used for analysis. For sections 102 and 103, enter the same parameters.

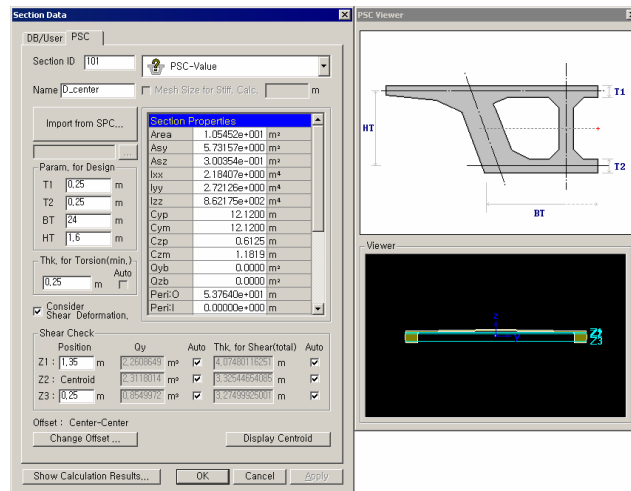


Figure 7. Input dimensions for PC box section

• **PC Sections**

ID	Type	Sub Type	Name	*.sec File Name	Remarks
101	PSC	PSC-Value	D_center	D_center.sec	Center part
102	PSC	PSC-Value	D_spt	D_suppot.sec	Support part
103	PSC	PSC-Value	D_py	D_py.sec	Tower part

• **Tower Sections**

ID	Type	Name	ID	Type	Name
201	Value	PY1_head	211	Value	PY2_head
202	Value	PY1_top	212	Value	PY2_top
203	Value	PY1_down	213	Value	PY2_down
204	DB/User	PY1_cross	214	DB/User	PY2_cross
205	DB/User	PY1_footing	215	DB/User	PY2_footing

• **Pier Sections**

Input 301~304 in Section ID in DB/User Type for modeling the pier sections.

• **Cable Sections**

401~409 sections to be used for cables are defined by Value Type. Import *.sec file to define the main girder sections. To define other sections, copy the data on the section tab of *Struc.xls* file and paste it into the section table. Classify Section Types into each tab as the type of data and the number of data are different from Section Type to Section Type.

Model / Properties / Section Table
DB/User tab ; Value tab

<DB/User Type>

ID	Name	Shape	DB	Section	Offset	OO type	Built-Up	Shear Deflect	Size 1 (mm)	Size 2 (mm)	Size 3 (mm)	Size 4 (mm)	Size 5 (mm)	Size 6 (mm)
204	PY1_cross	B	None	Center-Center			Built-Up	1	6	6	1	1	0	0
205	PY1_footing	B	None	Center-Center			Built-Up	1	24.6	31	0	0	0	0
214	PY2_cross	B	None	Center-Center			Built-Up	1	4.6	4.6	1	1	0	0
215	PY2_footing	B	None	Center-Center			Built-Up	1	18	28	0	0	0	0
301	P_top	B	None	Center-Center			Built-Up	1	3.2	3.36	0	0	0	0
302	P_down	B	None	Center-Center			Built-Up	1	3.2	3.36	0.7	0.7	0	0
303	P_cross	B	None	Center-Center			Built-Up	1	3.2	2.6	0	0	0	0
304	P_footing	B	None	Center-Center			Built-Up	1	11	20.6	0	0	0	0

Section

ID	Name	Shape	DB	Section	Offset	CC type	Built-Up	Shear Deflect	Size1 (m)
*									

Copy Paste Find... Ctrl+F

Figure 8. Section Table Input

Modeling of Structure

Input Nodes

Input node data in *Struc.xls* file and copy the node information from the file into the Node Tables.

Model / Nodes / **Node Tables**

To copy and paste Node Data into Node Table, activate the Node Column as shown below. Right-click over the Node column and select "Enable Edit". Now the Node column becomes enabled.

Node	X(m)	Y(m)	Z(m)

Copy the Node Data from the MS-Excel file and input it in the Table.

Node No.	X(m)	Y(m)	Z(m)
101	0.200005	0	-0.120999
102	0.950005	0	-0.080931
103	3.49908	0	-0.02553
104	5.49796	0	0.037519
105	7.39972	0	0.045447
106	9.60077	0	0.087961
107	11.2969	0	0.187265
108	14.5967	0	0.262128
109	16.2967	0	0.328129
110	17.9967	0	0.394131
111	21.2967	0	0.460133
112	24.5967	0	0.521044
113	26.2967	0	0.581956
114	27.9967	0	0.642868

Node	X(m)	Y(m)	Z(m)
101	0.200005	0.000000	-0.120999
102	0.950005	0.000000	-0.080931
103	3.499080	0.000000	-0.025530
104	5.497960	0.000000	0.037519
105	7.399720	0.000000	0.045447
106	9.600770	0.000000	0.087961
107	11.296900	0.000000	0.187265
108	14.596700	0.000000	0.262128
109	16.296700	0.000000	0.328129
110	17.996700	0.000000	0.394131
111	21.296700	0.000000	0.460133

Figure 9. Node Information and Input Table

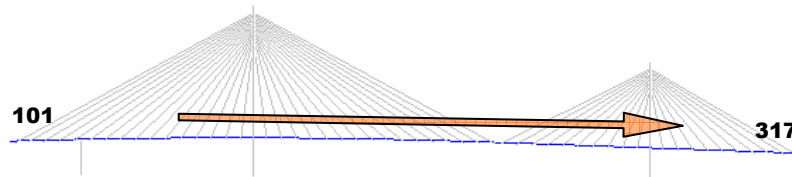
Input Elements

Likewise, enable the Element No. Column for pasting the data into the table. Copy the Element Data from Excel File and paste it into the table.

Model / Nodes / **Element Tables**

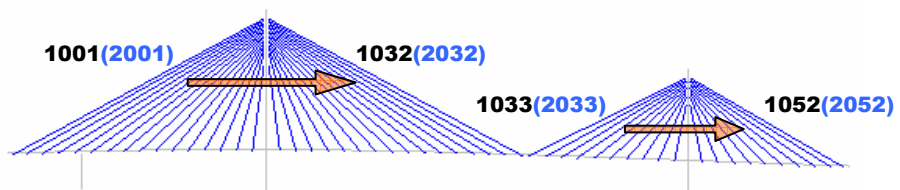
• Main girders

Main girder numbers are 101 ~ 317 from the left.


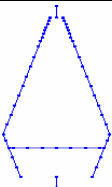
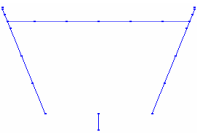


• Cable

Cable numbers are 1001 ~ 1032, 2001 ~ 2052 from the left. Numbers in parenthesis indicate the rear cables.




• Tower and Pier.


Main tower	Small tower	Pier
		
501to561	601to656	701to719

Input Boundary Conditions

Input Supports

Input the supports as shown in the figure below.

Model / Boundary /  **Supports**

 **Select Single** (Node: **389, 390, 397, 398, 2311, 2780, 3106**)

Support Type>**Dx** (on), **Dy** (on), **Dz**(on), **Rx** (on), **Ry** (on), **Rz**(on) ↵

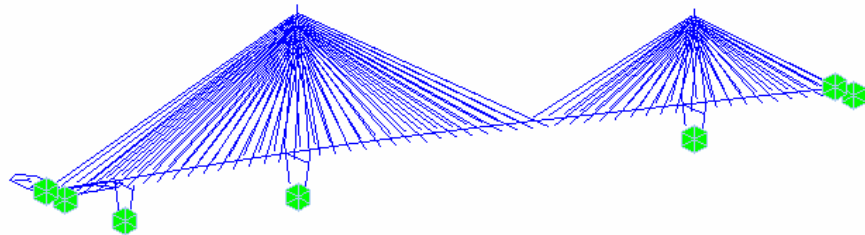


Figure 10. Input Supports

Input Beam End Offsets

Input the width of Beam End Offset at the pier step.

Model / Boundary / **Beam End Offset**

[Unit: m]							
Elem	Type	RGDXi	RGDYi	RGDZi	RGDXj	RGDYj	RGDZj
710	Global	0.0	1.72	0.0	0.0	0.0	0.0
715	Global	0	0	0	0	-1.72	0

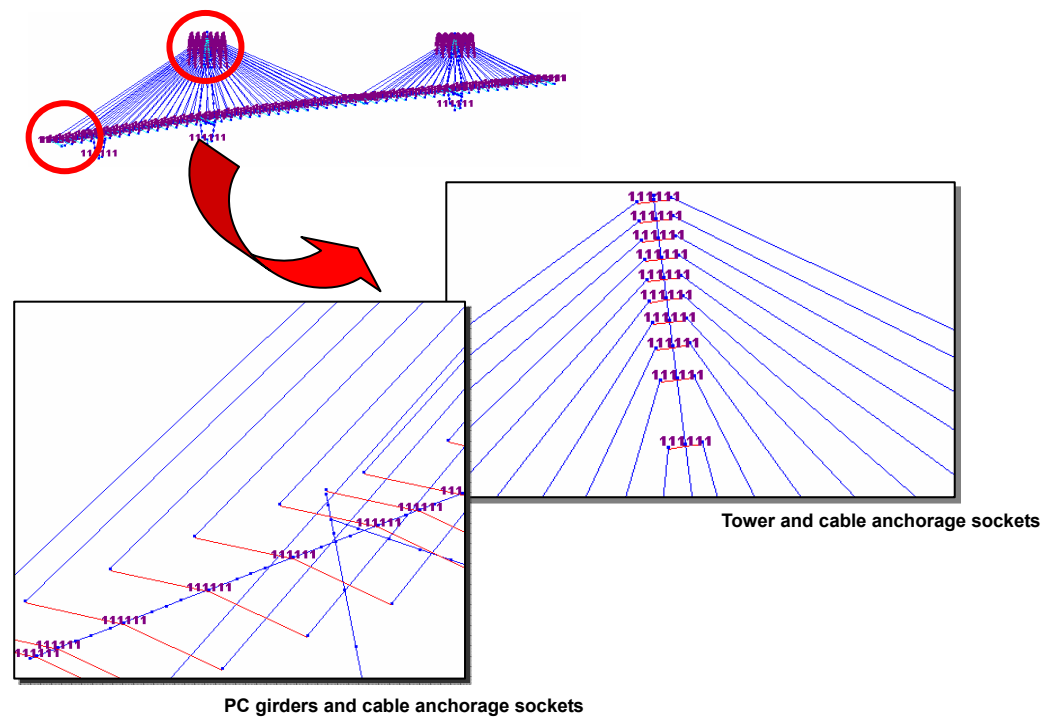
Rigid body connection

Enter rigid body connections between the main girders and cable anchorages, and between the towers and cable anchorages. Copy the data on Rigid Link tab of *Struc.xls* and paste it into Rigid Link Table.

Model / Boundary / **Rigid Link Table**

Input rigid body connections at the following locations.

- PC girders, towers and cable anchorages



Modeling Bridge Supports

Input Elastic Links at bridge supports connecting the bridge superstructure to the substructure.

Model / Boundary / **Elastic Link**

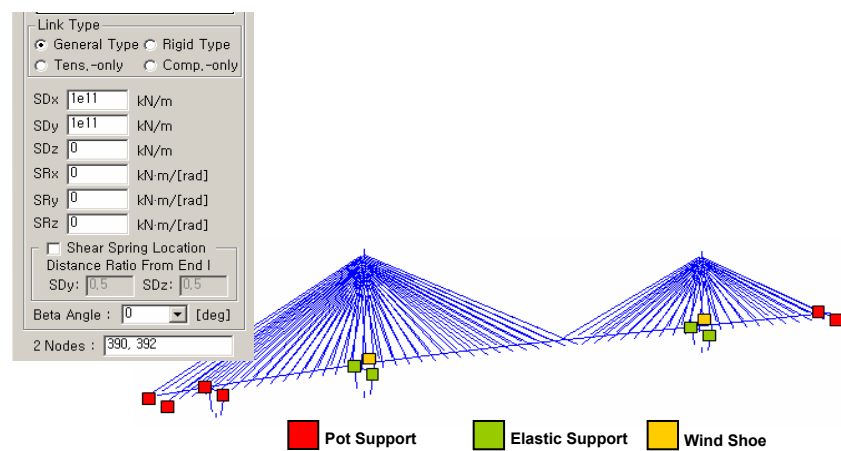


Figure 11. Locations for Installing Bridge Supports

Input the data for elastic links at the bridge supports as shown in the table below:

[Unit: kN, m]

No.	Node1	Node2	Type	SDx	SDy	SDz	Remarks
1	390	392	GEN	1E+11	1E+11	0	Pot support
2	389	391	GEN	1E+11	1E+11	0	Pot support
3	567	394	GEN	25230100	20670	20670	Elastic support
4	561	393	GEN	25230100	20670	20670	Elastic support
5	667	396	GEN	23870000	19810	19810	Elastic support
6	661	395	GEN	23870000	19810	19810	Elastic support
7	398	400	GEN	1E+11	1E+11	0	Pot support
8	397	399	GEN	1E+11	1E+11	0	Pot support
9	1009	168	GEN	0	7808220	0	Wind Shoe
10	1010	275	GEN	0	7808220	0	Wind Shoe
11	3013	3015	GEN	1E+11	1E+11	0	Pot support
12	3012	3014	GEN	1E+11	1E+11	0	Pot support

Input Loads

Define Loading Conditions

The loading conditions used in the analysis are defined.

 **Redraw**

Load /  **Static Load Cases**

Name (Self) ; Type>Dead Load (D) ↵
Name (2nd Dead) ; Type>Dead Load (D) ↵
Name (Cross W't) ; Type>Dead Load (D) ↵
Name (Pre01) ; Type>Prestress (PS) ↵
Name (Pre02) ; Type>Prestress (PS) ↵
Name (Pre03) ; Type>Prestress (PS) ↵

...

Name (Pre52) ; Type>Prestress (PS) ↵

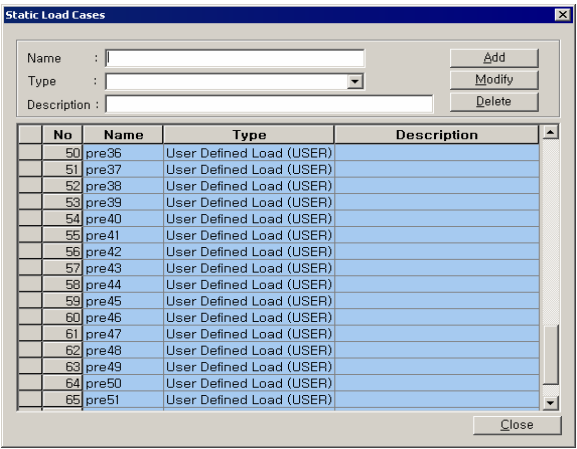



Figure 12. Define Load Case Dialog Box



Input Self Weight

Input the self weight as follows.

Load /  **Self Weight**
 Load Case Name>**Self**
 Load Group Name>**Self**
 Self Weight Factor>**Z (-1)** ↵

Superimposed Dead Load

Then apply the 2nd dead load by inputting it as Element Beam Load.

Load /  **Element Beam Loads**
 101to317 **101to317** ↵
 Load Case Name>**2nd Dead**
 Load Group Name>**2nd Dead**
 Load Type>**Uniform Loads**
 Value
 Relative ; x1(**0**) ; x2 (**1**) ; w (**-56.633**)

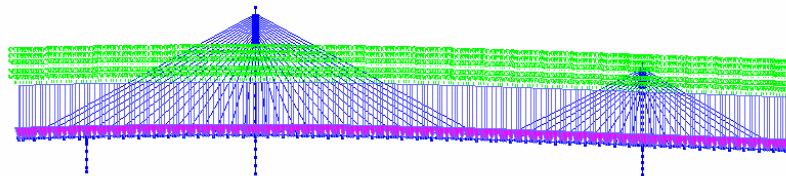


Figure 13. Apply 2nd Dead Load

Self weight of Cross Beams


Enter the weight of cross beams, which was excluded from the modeling, using nodal loads. Copy the loading information from the Load tab in *Struc.xls* and paste it into Nodal Load Table.

Load / Load Tables / Nodal Loads

Input Pretension Loads


Since this cable-stayed bridge has two sides, which are transversely symmetrical, identical initial pretensions in the cables on both sides will be introduced symmetrically to the bridge center. Therefore, we will input identical loading conditions to the cable pairs that form the transverse symmetry.

Load / Prestress Loads / Pretension Loads

 **Select Intersect** (Elements: **1001, 2001**)

Load Case Name > **Pre01**; Load Group Name > **Default**


Options > **Add**; Pretension Load (**1**) ↵

 **Select Intersect** (Elements: **1002, 2002**)

Load Case Name > **Pre02**; Load Group Name > **Default**

Options > **Add**; Pretension Load (**1**) ↵

...

 **Select Intersect** (Elements: **1052, 2052**)

Load Case Name > **Pre 52**; Load Group Name > **Default**

Options > **Add**; **Pretension** Load (**1**) ↵

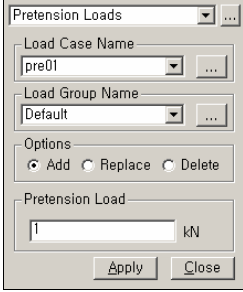
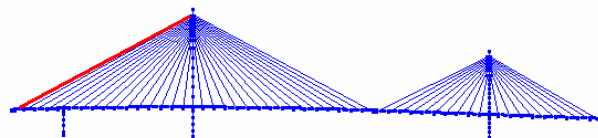



Figure 14. Input Pretension Loads

Perform Structural Analysis

After completing all the processes for modeling and load input, structural analysis is performed.

Analysis /  Perform Analysis

Calculate Initial Pretensions

Create Load Combinations

Create a load combination from the 52 unit pretension load cases introduced to each cable, self weight load case, superimposed dead load case and cross beam self weight load case.

Results / *Combinations*

Load Combination List > Name> **LCB1**

LoadCase > **Self(ST)** ; Factor **(1.0)**

LoadCase > **2nd Dead(ST)** ; Factor **(1.0)**

LoadCase > **Cross W't(ST)** ; Factor **(1.0)**

LoadCase > **Pre01(ST)** ; Factor **(1.0)**

...

LoadCase > **Pre16(ST)** ; Factor **(250)**

LoadCase > **Pre17(ST)** ; Factor **(250)**

...

LoadCase > **Pre52(ST)** ; Factor **(1.0)** ↵

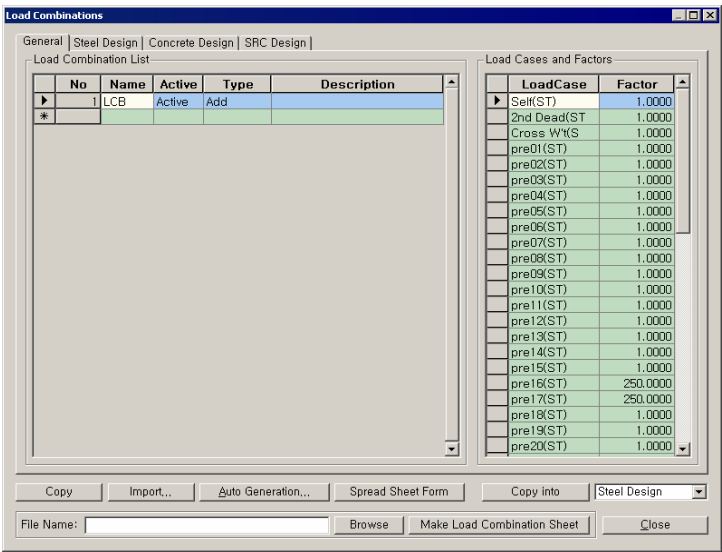


Figure 15. Input Load Combination

Calculate Unknown Load Factors

Calculate unknown load factors that satisfy the boundary conditions by the *Unknown Load Factor* function for LCB, which was generated through load combination. The constraints are specified to limit the deflections of the tower and the main girders.

Specify the load condition, constraints and method of forming the object function in *Unknown Load Factor*. First, we define the cable unit loading conditions as unknown loads.

Results / *Unknown Load Factor*

Unknown Load Factor Group > Add New

Item Name (**Unknown**) ; Load Comb > **LCB**

Object function type > **Square** ; Sign of unknowns > **Both**

LCase > **Pre01** (on)

...

LCase > **Pre15** (on)

LCase > **Pre18** (on)

...

LCase > **Pre52** (on)

Item Name: Unknown

Load Comb: LCB

Object function type: ☐ Linear ☒ Square ☐ Max Abs

Sign of unknowns: ☐ Negative ☒ Both ☐ Positive

Constraints:

- ☐ M501
- ☐ M601
- ☒ py101
- ☐ py102
- ☐ py103
- ☐ py104
- ☐ py105

Buttons: Add New Constraint, Modify, Delete

	Unknown	LCase	Factor	Weighted Factor
1	<input type="checkbox"/>	Self	1,000	
2	<input type="checkbox"/>	2nd Dead	1,000	
3	<input type="checkbox"/>	Cross W't	1,000	
4	<input checked="" type="checkbox"/>	pre01	Unknown	1.0
5	<input checked="" type="checkbox"/>	pre02	Unknown	1.0
6	<input checked="" type="checkbox"/>	pre03	Unknown	1.0
7	<input checked="" type="checkbox"/>	pre04	Unknown	1.0
8	<input checked="" type="checkbox"/>	pre05	Unknown	1.0

☐ Simultaneous Equations Method

Buttons: Select All, Unselect All, Get Unknown Load Factors, OK, Cancel

Figure 16. Unknown Load Factors

Specify the constraint conditions, which restrict the displacements of the tower and the main girders by using the **Constraints** function.

🔊 The boundary conditions for the Unknown Load Factors can also be applied through the MCT Command Shell.

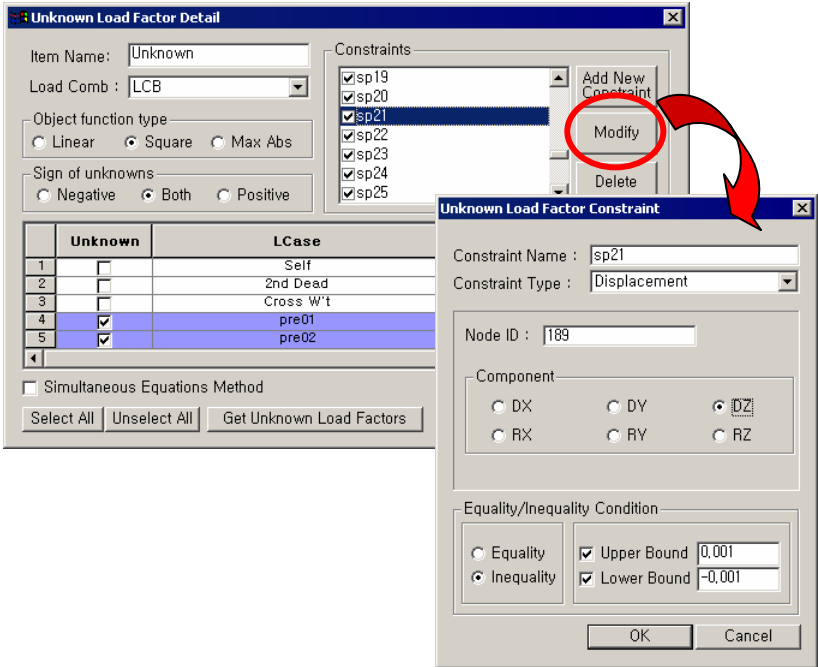


Figure 17. Input Constraint Conditions

Refer to the table below for inputting the constraint conditions for calculating the unknown load factors.

[Unit: m]

No	Node1	Node2	Type	SDx	SDy	SDz
py101	DISP	554	RY	Inequality	1.00E-06	-1.00E-06
py201	DISP	645	RY	Inequality	1.00E-06	-1.00E-06
sp01	DISP	103	DZ	Inequality	-0.001	0.001
sp02	DISP	107	DZ	Inequality	0.001	-0.001
sp03	DISP	111	DZ	Inequality	0.001	-0.001
sp04	DISP	115	DZ	Inequality	0.001	-0.001
sp05	DISP	119	DZ	Inequality	0.001	-0.001
sp06	DISP	123	DZ	Inequality	0.001	-0.001
sp07	DISP	127	DZ	Inequality	0.001	-0.001
sp08	DISP	131	DZ	Inequality	0.001	-0.001
sp09	DISP	135	DZ	Inequality	0.001	-0.001
sp10	DISP	139	DZ	Inequality	0.001	-0.001
sp11	DISP	143	DZ	Inequality	0.001	-0.001
sp12	DISP	147	DZ	Inequality	0.001	-0.001
sp13	DISP	151	DZ	Inequality	0.001	-0.001
sp14	DISP	155	DZ	Inequality	0	-0.001
sp15	DISP	159	DZ	Inequality	0	-0.001
sp16	DISP	163	DZ	Inequality	0.001	-0.001
sp17	DISP	173	DZ	Inequality	0.001	-0.001
sp18	DISP	177	DZ	Inequality	0	-0.001
sp19	DISP	181	DZ	Inequality	0	-0.001
sp20	DISP	185	DZ	Inequality	0.001	-0.001
sp21	DISP	189	DZ	Inequality	0.001	-0.001
sp22	DISP	193	DZ	Inequality	0.001	-0.001
sp23	DISP	197	DZ	Inequality	0.001	-0.001
sp24	DISP	201	DZ	Inequality	0.001	-0.001
sp25	DISP	205	DZ	Inequality	0.001	-0.001
sp26	DISP	209	DZ	Inequality	0.001	-0.001
sp27	DISP	213	DZ	Inequality	0.001	-0.001
sp28	DISP	217	DZ	Inequality	0.001	-0.001
sp29	DISP	221	DZ	Inequality	0.001	-0.001
sp30	DISP	225	DZ	Inequality	0.001	-0.001
sp31	DISP	229	DZ	Inequality	0.001	-0.001
sp32	DISP	233	DZ	Inequality	0.001	-0.001
sp33	DISP	234	DZ	Inequality	0.001	-0.001
sp34	DISP	238	DZ	Inequality	0.001	-0.001
sp35	DISP	242	DZ	Inequality	0.001	-0.001
sp36	DISP	246	DZ	Inequality	0.001	-0.001
sp37	DISP	250	DZ	Inequality	0.001	-0.001

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sp38	DISP	254	DZ	Inequality	0.001	-0.001
sp39	DISP	258	DZ	Inequality	0	-0.001
sp40	DISP	262	DZ	Inequality	0	-0.001
sp41	DISP	266	DZ	Inequality	0	-0.001
sp42	DISP	270	DZ	Inequality	0.001	-0.001
sp43	DISP	280	DZ	Inequality	0.001	-0.001
sp44	DISP	284	DZ	Inequality	0	-0.001
sp45	DISP	288	DZ	Inequality	0	-0.001
sp46	DISP	292	DZ	Inequality	0	-0.001
sp47	DISP	296	DZ	Inequality	0.001	-0.001
sp48	DISP	300	DZ	Inequality	0.001	-0.001
sp49	DISP	304	DZ	Inequality	0.001	-0.001
sp50	DISP	308	DZ	Inequality	0.001	-0.001
Sp51	DISP	312	DZ	Inequality	0.001	-0.001

Refer to the portion on the optimization technique of unknown loads for an explanation on calculation of Unknown Load Factors given in "Analysis for Civil Structures".

We now check the constraints used to calculate the cable initial pretensions and unknown load factors in *Unknown Load Factor Result*.

Unknown Load Factor Group > [Get Unknown Load Factors !](#)

Figure 18 shows the analysis results for calculating the Unknown Load Factors.

🔊 **Make Load Combination** uses the Unknown Load Factors which are automatically created for the Load Combination.

🔊 **Generate the Influence Matrix** as a MS-Excel File from the calculation results of Unknown Load Factors.

	Self	2nd Dead	Cross W't	pre01	pre02	pre03	pre04	pre05
Factor	1,000	1,000	1,000	391,192	489,373	582,437	569,723	328,291
Constraint	py101	py201	sp02	sp03	sp04	sp05	sp06	sp07
Value	0,000	-0,000	-0,001	-0,001	-0,001	-0,001	-0,001	-0,000
Upper Bound	0,000	0,000	0,001	0,001	0,001	0,001	0,001	0,001
Lower Bound	-0,000	-0,000	-0,001	-0,001	-0,001	-0,001	-0,001	-0,001

Figure 18. Unknown Load Factor Calculation Results

We will now check whether the calculation results satisfy the constraints by auto-generating a new load combination using the unknown load factors in the **Make Load Combination** function.

Figure 19. Automatic generation of "ULF" load combination using the unknown load factors

Confirm the results of the load combination that is automatically generated using the unknown load factors.

Results / *Combinations*

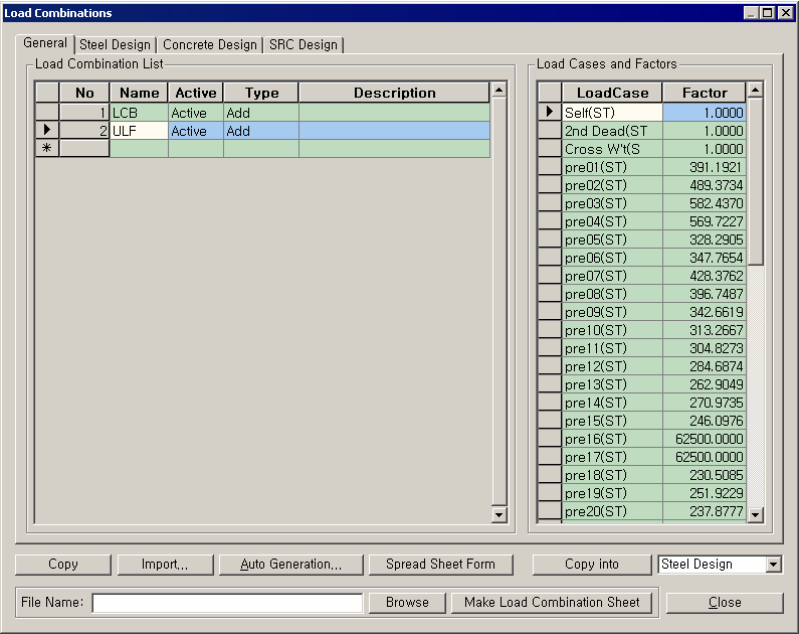



Figure 20. Automatic Generation of “ULF” Load Combination that uses the Unknown Load Factors

Review Analysis Results

Review deformed shape.

Review the deformed shape for the “ULF” load combination calculated from the initial pre-tensions using the Unknown Load Factors.

Result / Deformations /  **Deformed Shape**
Load Cases / Combinations > **CB:ULF**
Components > **DZ**
Type of Display > **Undeformed (on)** ; **Legend (on)**

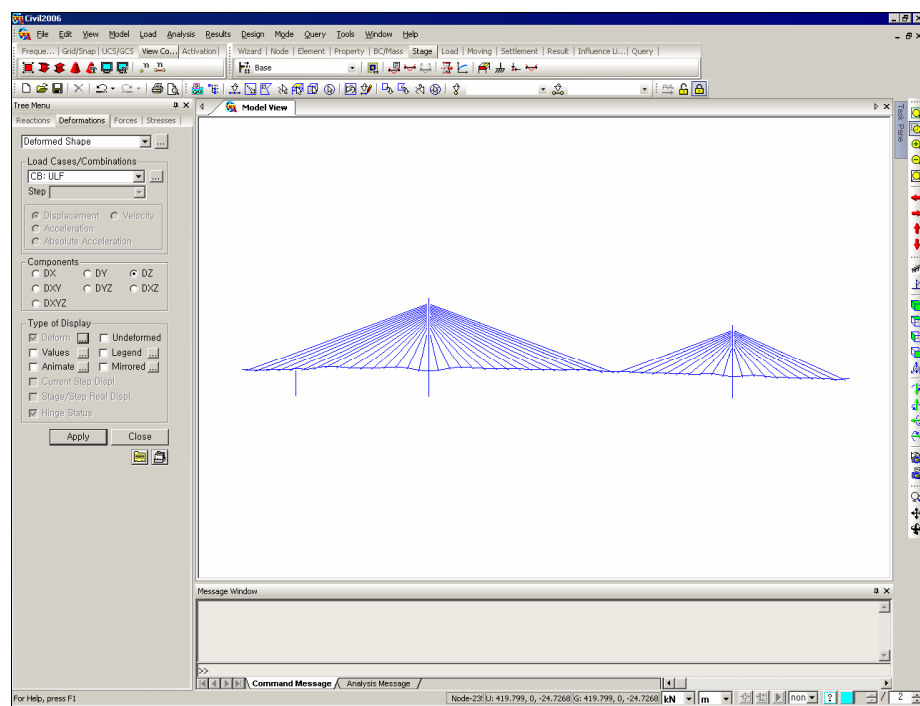


Figure 21. Deformed Shape Results

Review Member Forces

Review the member forces for the “ULF” load combination.

Result / Force / Beam Diagram

Load Cases / Combinations > **CB:ULF**

Components > **DXYZ**

Type of Display > **Undeformed (on)** ; **Legend (on)**

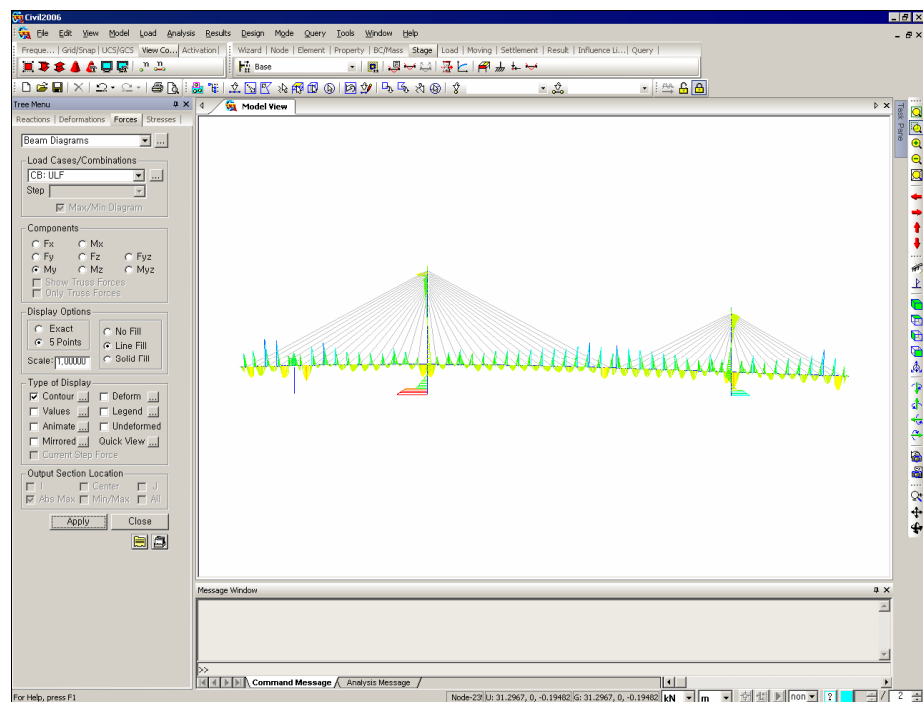


Figure 22. Review Member Forces